

# **EE1 and ISE1 Communications I**

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Lecture fifteen

# Lecture Aims

- To identify how resilient FM is to non-linear distortion
- To outline FM modulators and demodulators

## Angle Modulation and non-linearities

- FM signals are constant envelope signals, therefore they are less susceptible to non-linearities
- Example: a non linear device whose input  $x(t)$  and output  $y(t)$  are related by

$$y(t) = a_1x(t) + a_2x^2(t)$$

- if  $x(t) = \cos[\omega_c t + \psi(t)]$

- Then

$$\begin{aligned}y(t) &= a_1 \cos[\omega_c t + \psi(t)] + a_2 \cos^2[\omega_c t + \psi(t)] \\ &= \frac{a_2}{2} + a_1 \cos[\omega_c t + \psi(t)] + \frac{a_2}{2} \cos[2\omega_c t + 2\psi(t)]\end{aligned}$$

## Angle Modulation and non-linearities

- For FM wave

$$\psi(t) = k_f \int m(\alpha) d\alpha$$

- The output waveform is

$$y(t) = \frac{a_2}{2} + a_1 \cos[\omega_c t + k_f \int m(\alpha) d\alpha] + \frac{a_2}{2} \cos[2\omega_c t + 2k_f \int m(\alpha) d\alpha]$$

- Unwanted signals can be removed by means of a bandpass filter

## Higher order non-linearities

- Consider higher order non-linearities

$$y(t) = a_0 + a_1x(t) + a_2x^2(t) + \dots + a_nx^n(t)$$

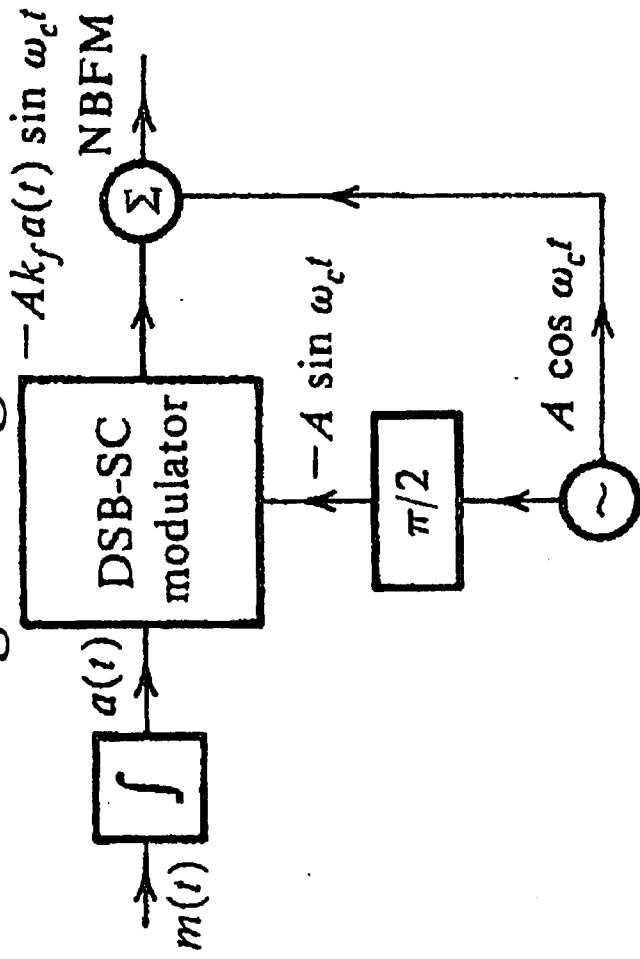
- If the input signal is an FM wave,  $y(t)$  will have the form

$$y(t) = c_0 + c_1 \cos [\omega_c t + k_f \int m(\alpha) d\alpha] + c_2 \cos [2\omega_c t + 2k_f \int m(\alpha) d\alpha] \\ + \dots + c_n \cos [n\omega_c t + nk_f \int m(\alpha) d\alpha]$$

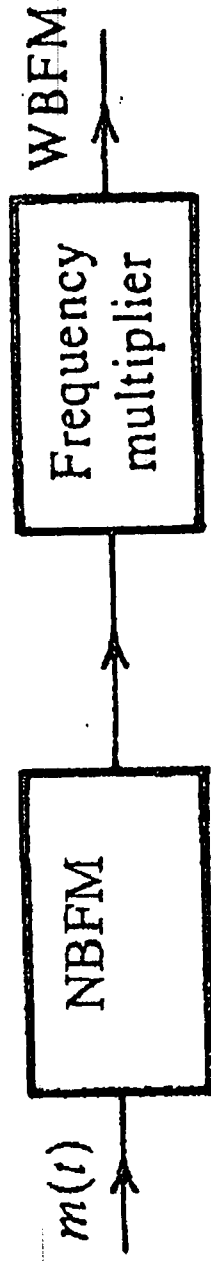
- The deviations are  $\Delta f, 2\Delta f, \dots, n\Delta f$

- **TRANSMISSIONS TECHNIQUE/METHOD OF FM GENERATION**

- **Narrowband signal is generated using**



- **NBFM signal is then converted to WBFM using**



## Direct Method of FM Generation

- The modulating signal  $m(t)$  can control a voltage controlled oscillator to produce instantaneous frequency

$$\omega_i(t) = \omega_c + k_f m(t)$$

- A voltage controlled oscillator can be implemented using an  $LC$  parallel resonant circuit with centre frequency

$$\omega_o = \frac{1}{\sqrt{LC}}$$

- If the capacitance is varied by  $m(t)$

$$C = C_0 - km(t)$$

## Direct Method of FM Generation

- The oscillator frequency is given by

$$\omega_i(t) = \frac{1}{\sqrt{LC_0 \left[ 1 - \frac{km(t)}{C_0} \right]}} = \frac{1}{\sqrt{LC_0} \left[ 1 - \frac{km(t)}{C_0} \right]^{1/2}}$$

- If  $\frac{km(t)}{C_0} \ll 1$ , the binomial series expansion gives

$$\omega_i(t) \simeq \frac{1}{\sqrt{LC_0}} \left[ 1 + \frac{km(t)}{2C_0} \right]$$

- This gives the instantaneous frequency as a function of the modulating signal.



## Demodulation of FM signals

- The FM demodulator is given by a differentiator followed by an envelope detector
- Output of the ideal differentiator

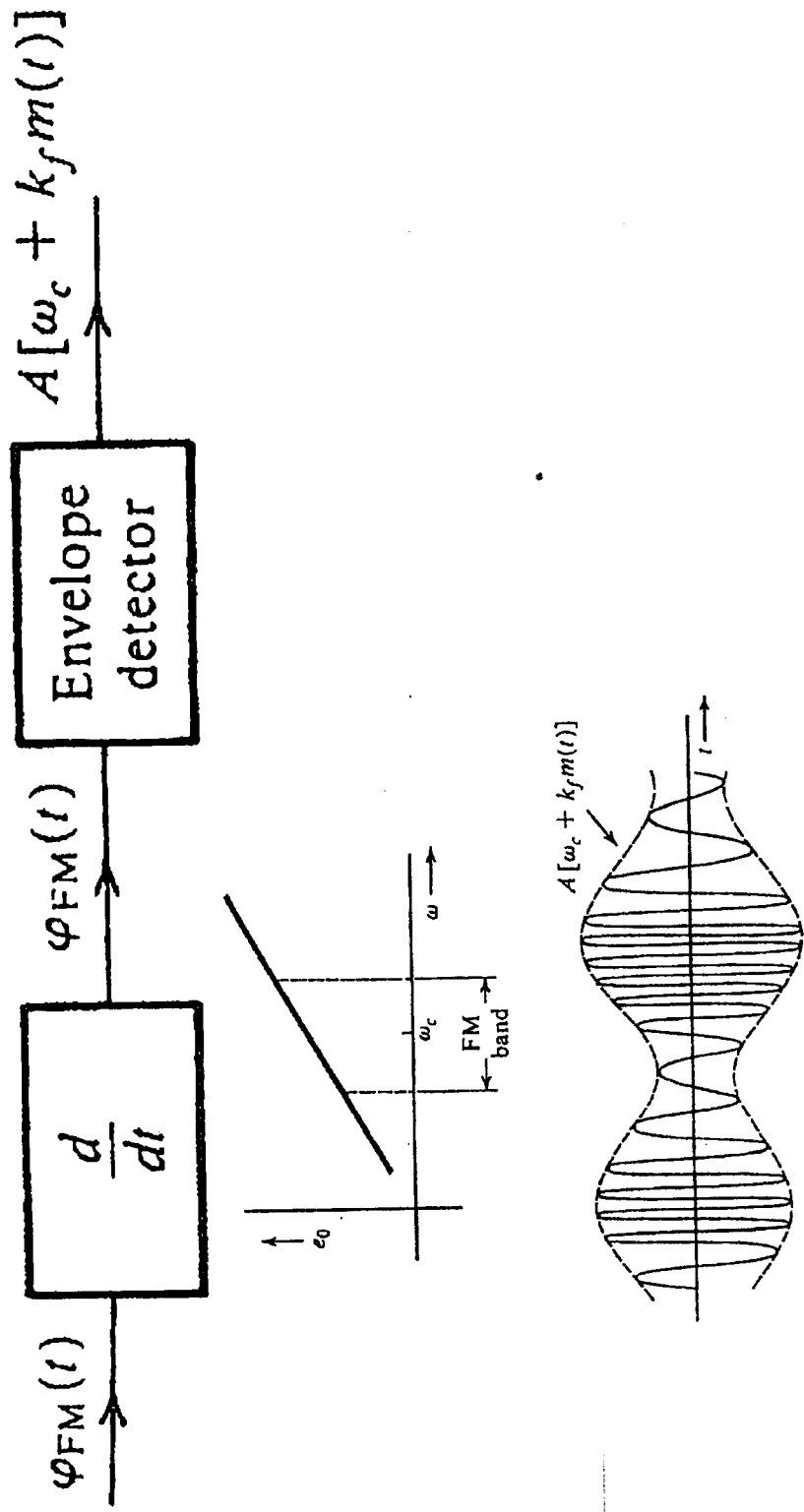
$$\begin{aligned}\dot{\phi}_{FM}(t) &= \frac{d}{dt} \left\{ A \cos \left[ \omega_c t + k_f \int_{-\infty}^t m(\alpha) d\alpha \right] \right\} \\ &= A[\omega_c + k_f m(t)] \sin \left[ \omega_c t + k_f \int_{-\infty}^t m(\alpha) d\alpha \right]\end{aligned}$$

- The above signal is both amplitude and frequency modulated. Hence, an envelope detector with input  $\dot{\phi}_{FM}(t)$  yields an output proportional to

$$A[\omega_c + k_f m(t)]$$

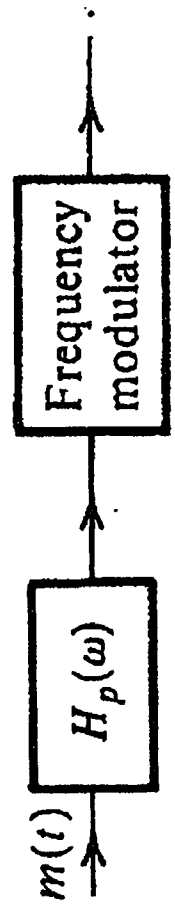
## Demodulation of FM signals

- As  $\Delta\omega = k_f m_D < \omega_c$  and  $\omega_c + k_f m(t) > 0$  for all  $t$ . The modulating signal  $m(t)$  can be obtained using an envelope detector.

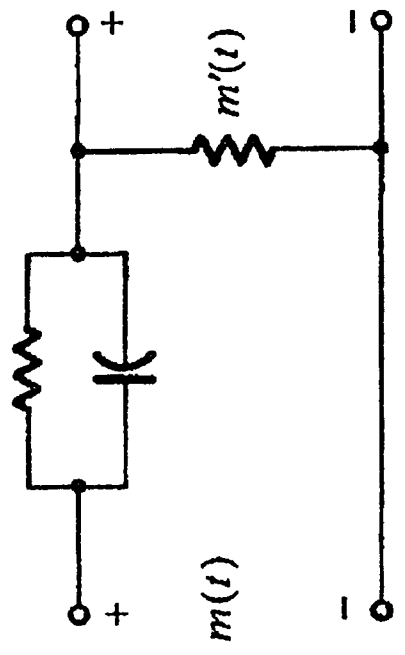
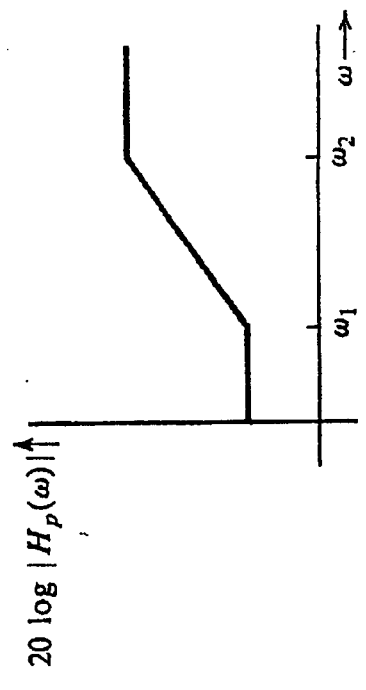


# Pre-emphasis and de-emphasis circuits

- To improve noise immunity of FM signals we use a pre-emphasis circuit at transmitter

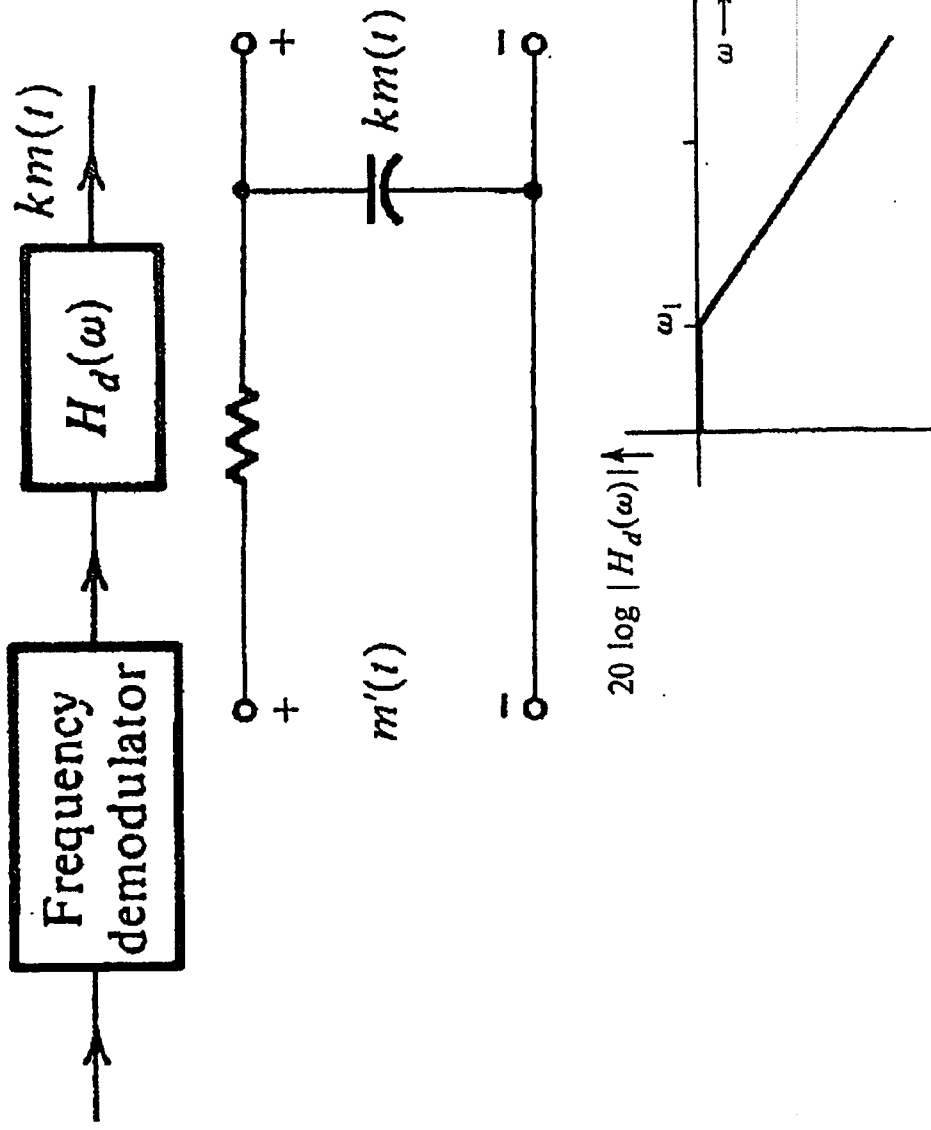


$$H_p(\omega) = K \frac{j\omega + \omega_1}{j\omega + \omega_2}$$

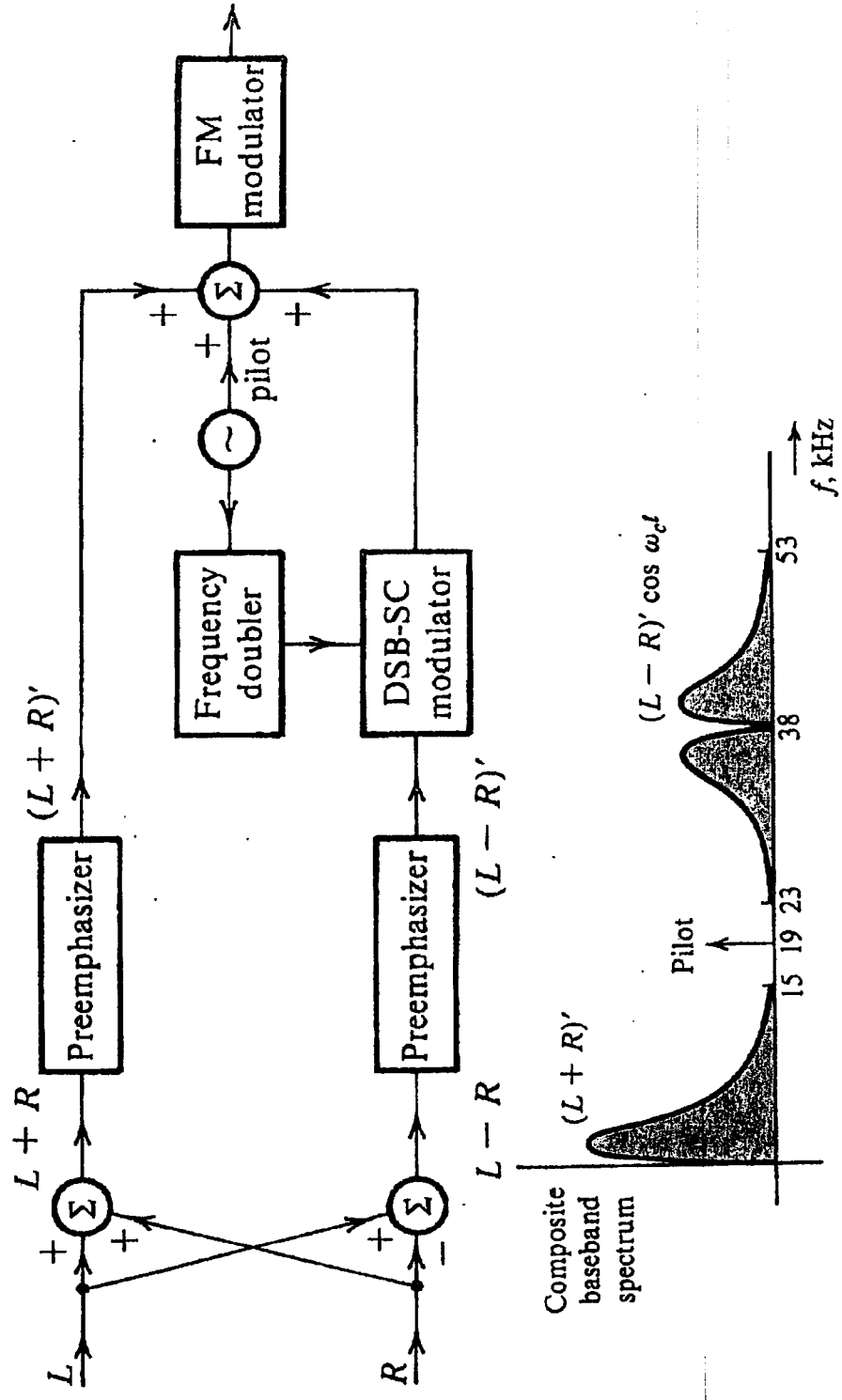


# De-emphasis circuit in receiver

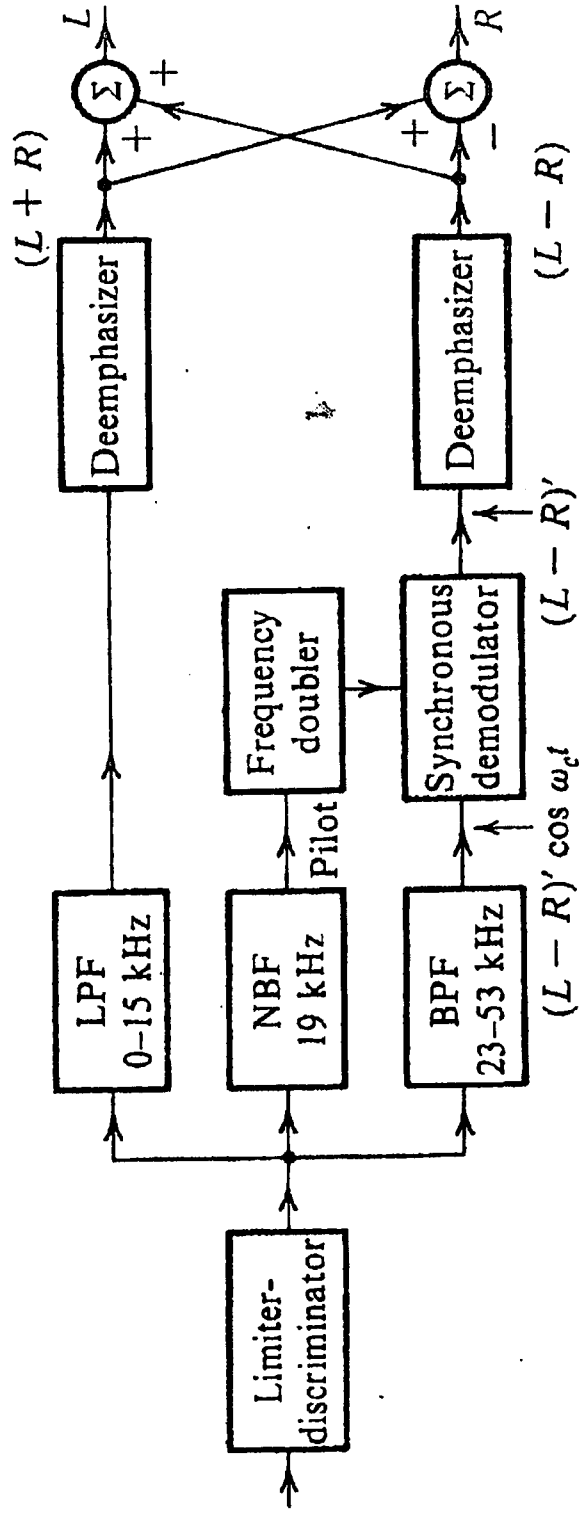
- Receiver de-emphasis circuit



# • Transmitter



# • Receiver



## Conclusions

- FM modulators: direct and indirect methods
- FM demodulator
- Pre-emphasis and de-emphasis circuits to improve noise immunity of signals
- FM stereo transmitter and receiver